

CO₂-injection modelling

Two-phase flow, poroelasticity,
dissolution of CO₂

Deep Saline Aquifers for Geological Storage of CO₂ and
Energy – IFP, Paris 27. – 29. May 2009

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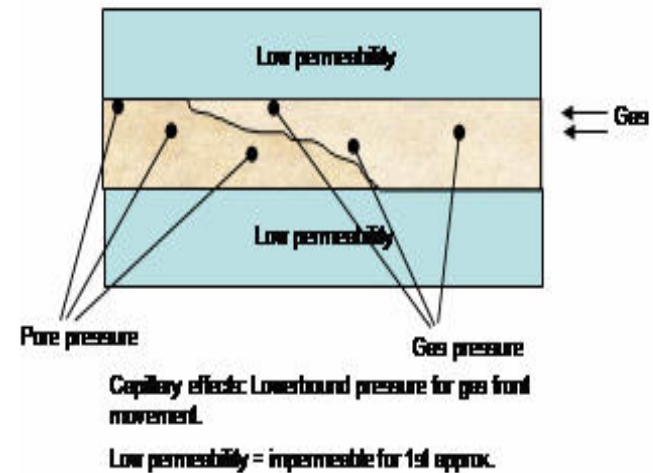
Agenda

- Background and motivation
- Short on CO₂ storage mechanisms
- Model review: equations and physics
- Examples, storage mechanisms:
 1. Comparing two viscosity ratios: 1. $\mu_w > \mu_n$, 2. $\mu_n > \mu_w$
 2. Solubility trapping: Comparing dissolution of CO₂ vs. no-dissolution
 3. Residual trapping
 4. Poroelasticity (including dissolution of CO₂)
 5. Calculating pH

Background and motivation

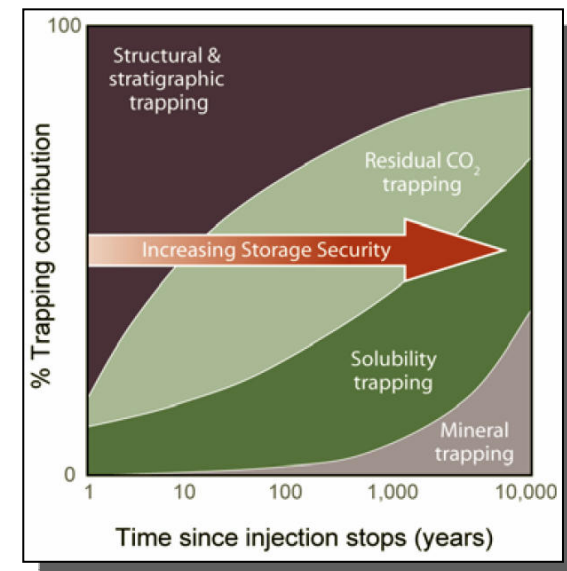
Two main areas of interest:

1. CO₂ Storage: focus on short term storage and the injection process
2. Gas flow into and out of a well; shallow gas seepage



CO₂ storage mechanisms

- Storage idea: Inject CO₂ into a **suitable** porous formation below an intact cap rock so that it will not **leak**
- Types of storage mechanism of CO₂:
 1. Structural trapping: Migration blocked by impermeable cap rock
 2. Residual trapping: CO₂ stabilized by capillary pressure
 3. Solubility trapping: In time CO₂ will dissolve in salt pore water (heavy, descends)
 4. Mineral trapping: In time CO₂ will chemically react with rock to form carbonates and precipitate



(From: IPCC Special report, 2005)

Modelling challenges

1. How does the CO₂ migrate in the formation, considering perforated/poorly plugged wells, faults, fractures, etc.
 - Two-phase flow (maybe even more phases)
2. How does CO₂ injection affect the rock
 - Poroelasticity
3. Chemical reactions and borehole integrity
 - Solubility of CO₂ in water
 - (Other effects are: chemical reaction with rock formation, corrosion, erosion, degradation of bore hole)

Model review

Equations and physics



Two-phase flow equations

$$\left. \begin{aligned} \frac{\partial}{\partial t}(\phi \rho_{\alpha} S_{\alpha}) - \nabla \cdot [\rho_{\alpha} \lambda_{\alpha} \mathbf{K}(\nabla p_{\alpha} + \gamma_{\alpha} \nabla z)] &= \rho_{\alpha} q_{\alpha} \\ \sum S_{\alpha} &= 1, \quad p_c = p_n - p_w, \quad S_{e\alpha} = f(p_c) \end{aligned} \right\} \begin{array}{l} \text{General mass} \\ \text{balances and} \\ \text{auxiliary} \\ \text{equations} \end{array}$$

Two-phase flow equations

$$\left. \begin{aligned} \frac{\partial}{\partial t}(\phi \rho_{\alpha} S_{\alpha}) - \nabla \cdot [\rho_{\alpha} \lambda_{\alpha} \mathbf{K}(\nabla p_{\alpha} + \gamma_{\alpha} \nabla z)] &= \rho_{\alpha} q_{\alpha} \\ \sum S_{\alpha} &= 1, \quad p_c = p_n - p_w, \quad S_{e\alpha} = f(p_c) \end{aligned} \right\} \begin{array}{l} \text{General mass} \\ \text{balances and} \\ \text{auxiliary} \\ \text{equations} \end{array}$$

⇓

Do some equation manipulation: Fractional flow formulation

(The fractional flow approach treats the multiphase flow problem as a total fluid flow of a single mixed fluid, and then describes the individual phases as fractions of the total flow)

Two-phase flow equations

$$\left. \begin{aligned} \frac{\partial}{\partial t} (\phi \rho_\alpha S_\alpha) - \nabla \cdot [\rho_\alpha \lambda_\alpha \mathbf{K} (\nabla p_\alpha + \gamma_\alpha \nabla z)] &= \rho_\alpha q_\alpha \\ \sum S_\alpha &= 1, \quad p_c = p_n - p_w, \quad S_{e\alpha} = f(p_c) \end{aligned} \right\} \begin{array}{l} \text{General mass} \\ \text{balances and} \\ \text{auxiliary} \\ \text{equations} \end{array}$$

$$\begin{aligned} \nabla \cdot \mathbf{u} &= q_w + q_n - \frac{1}{\rho_w} \frac{\partial \rho_w}{\partial p} \left(\frac{\partial p}{\partial x} u_{w,x} + \frac{\partial p}{\partial y} u_{w,y} - \frac{\partial p}{\partial t} \phi S_w \right) - \frac{1}{\rho_n} \frac{\partial \rho_n}{\partial p} \left(\frac{\partial p}{\partial x} u_{n,x} + \frac{\partial p}{\partial y} u_{n,y} - \frac{\partial p}{\partial t} \phi S_n \right) - \frac{\partial \phi}{\partial t} \\ \phi \rho_w \frac{\partial S_w}{\partial t} + \nabla \cdot (\rho_w \mathbf{u}_w) &= \rho_w q_w - \phi S_w \frac{\partial \rho_w}{\partial p} \frac{\partial p}{\partial t} - \rho_w S_w \frac{\partial \phi}{\partial t} \end{aligned}$$

$$\mathbf{u} = -\mathbf{K} (\lambda \nabla p - (\lambda_w \rho_w + \lambda_n \rho_n) \mathbf{g})$$

$$\mathbf{u}_w = f_w \mathbf{u} + \lambda_n f_w K (\nabla p_c + (\rho_w - \rho_n) \mathbf{g})$$

$$\mathbf{u}_n = f_n \mathbf{u} - \lambda_n f_w K (\nabla p_c + (\rho_w - \rho_n) \mathbf{g})$$

Biot linear poroelasticity equation

Flow coupled to geomechanics

$$\nabla \cdot [\boldsymbol{\sigma}] = -\mathbf{F}$$

$$\boldsymbol{\sigma} = \mathbf{D}_{el} \boldsymbol{\varepsilon} - \alpha_{biot} p \mathbf{I}$$

Geomechanics coupled to flow:

$$\phi^* = (1 - \varepsilon_v) \phi$$

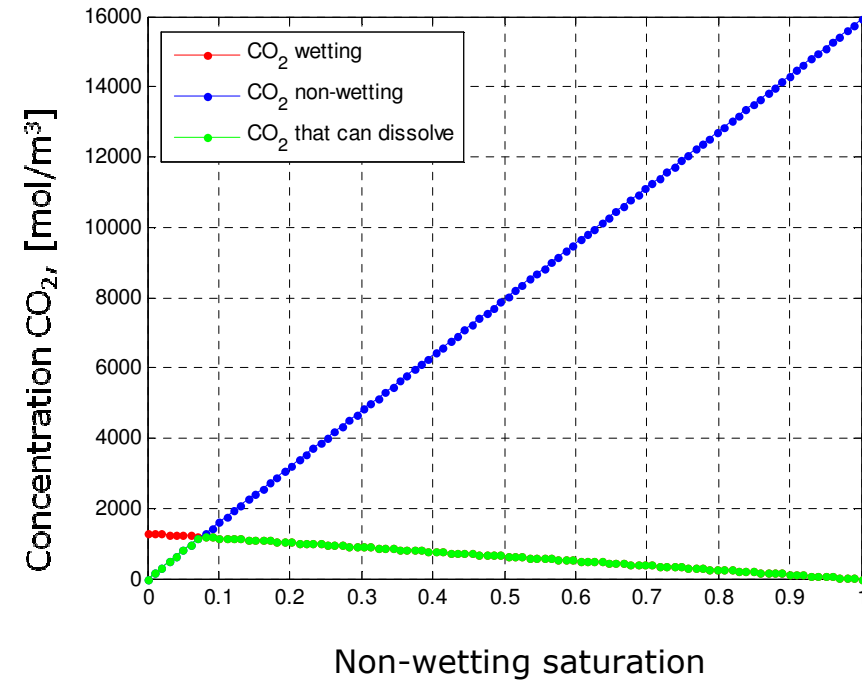
$$K = K_0 \left(\frac{\phi^*}{\phi} \right)^{3.4} \quad (\text{vary from case to case})$$



Mass balance equation, CO₂(aq)

$$\frac{\partial C_{CO_2}}{\partial t} + \nabla \cdot (-D \nabla C_{CO_2}) = F$$

$$F = k_s (\min(C_{sat,CO_2} S_w, C_{0,CO_2} S_n) - C_{CO_2})$$



C_{sat,CO_2} – saturated concentration of CO₂ in water; CO₂(aq) [mol/m³]
 C_0 – concentration of pure CO₂ [mol/m³]

pH calculation

$\text{CO}_2(\text{sc}) \rightleftharpoons \text{CO}_2(\text{aq})$, dissolution (sc – super critical)

$\text{CO}_2(\text{aq}) + \text{H}_2\text{O}(\text{l}) \rightleftharpoons \text{H}_2\text{CO}_3(\text{aq})$, hydration

Treating $\text{CO}_2(\text{aq})$ and $\text{H}_2\text{CO}_3(\text{aq})$ as one entity, CO_2^* :

$\text{CO}_2^* + \text{H}_2\text{O} \rightleftharpoons \text{HCO}_3^-(\text{aq}) + \text{H}_3\text{O}^+(\text{aq})$, first dissociation, $\text{p}K_{a1}$

$\text{HCO}_3^-(\text{aq}) \rightleftharpoons \text{CO}_3^{2-}(\text{aq}) + \text{H}_3\text{O}^+(\text{aq})$, second dissociation, $\text{p}K_{a2}$

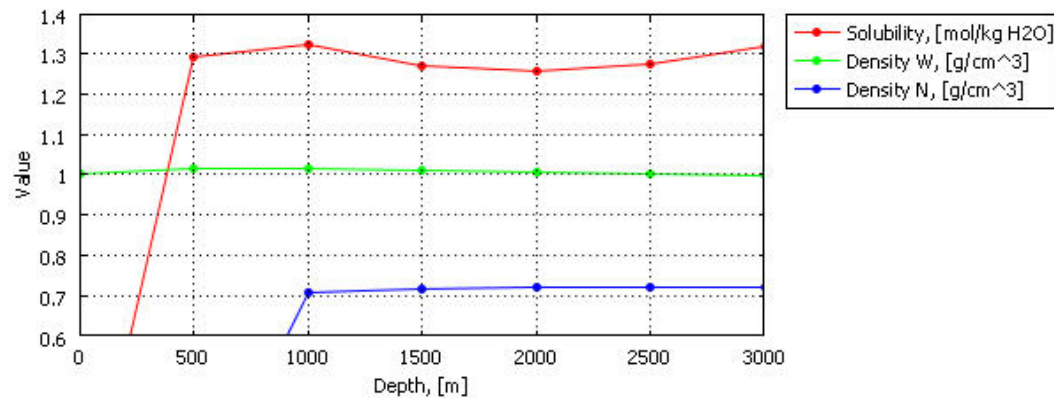
Using:

- Protolysis constants, K_{a1} and K_{a2}
- Stoichiometric relation for initial concentration c of carbonic acid
- Water constant, K_w
- Electro neutrality

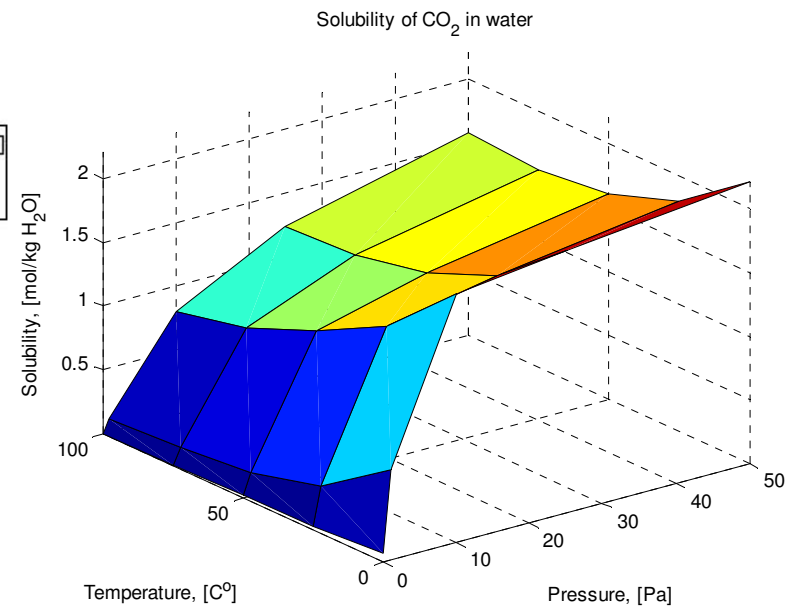
⇒ Four equation, four unknowns:
$$\text{pH} = -\log_{10}(\sqrt{K_{a1}c + K_{a2}c + K_w})$$

CO₂ density and solubility

Symbol	Value	Unit	Description
ρ_{H2O}	1000	[kg/m ³]	Density of water-phase
ρ_{CO2}	700	[kg/m ³]	Density of CO ₂ -phase
C_{sat}	1300	[mol/m ³]	Saturation concentration of CO ₂ in water



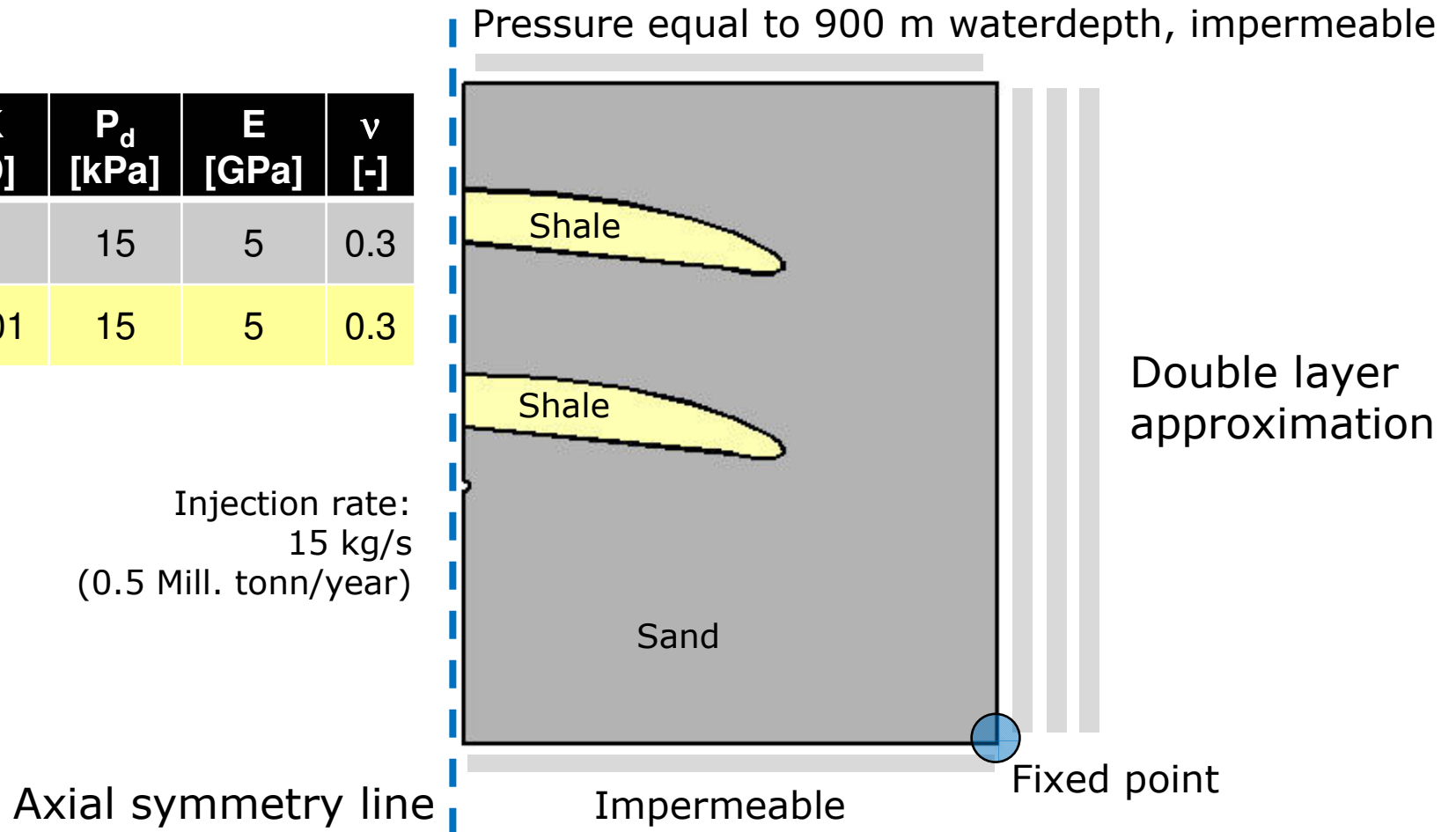
(Temperature gradient used: 28K/km)



Model (200 x 250 m²), axial symmetry

ϕ [-]	K [D]	P_d [kPa]	E [GPa]	ν [-]
0.42	1	15	5	0.3
0.1	0.01	15	5	0.3

Injection rate:
15 kg/s
(0.5 Mill. tonn/year)



Examples

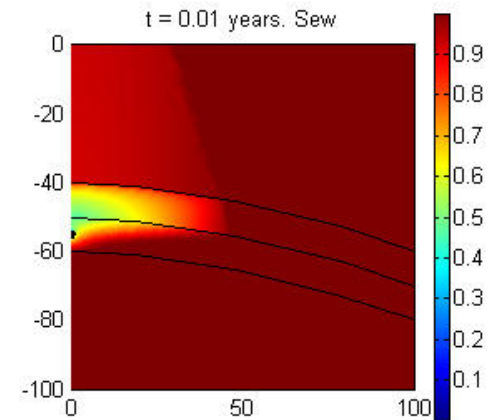
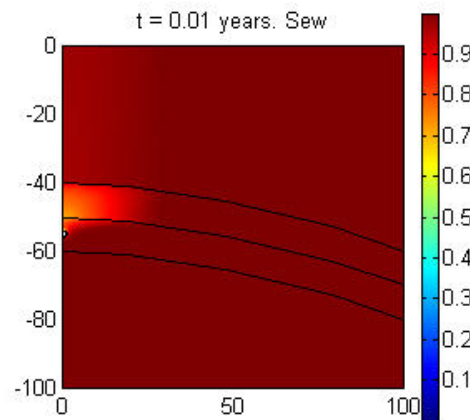
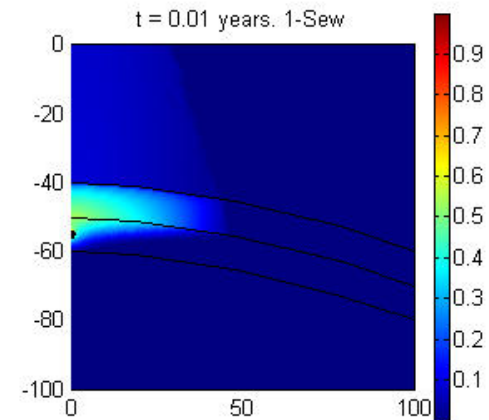
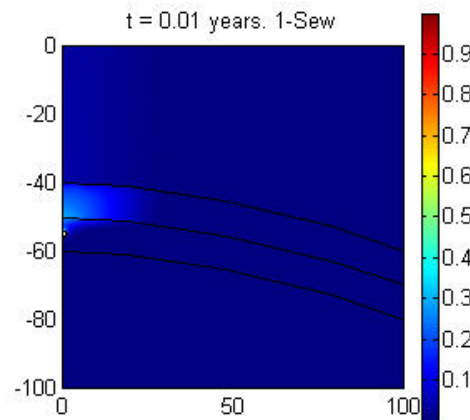
Storage mechanisms



Example 1: Viscosity ratios

High value:
0.5 mPa·s

Low value:
0.05 mPa·s



Example 1: Viscosity ratios, version 2

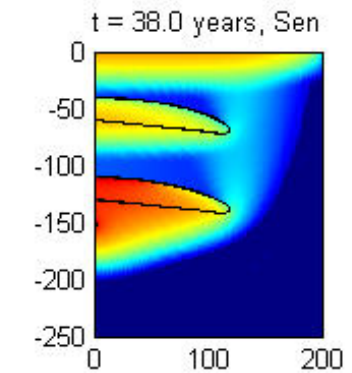
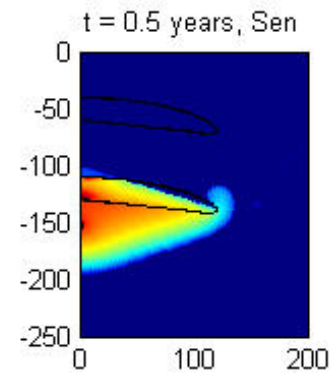
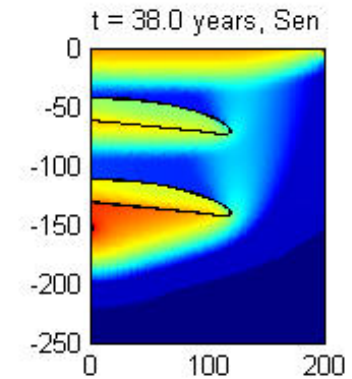
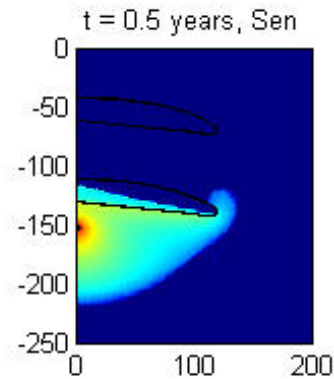
CO₂ constant

Water high:
5 mPa·s

CO₂ low:
0.5 mPa·s

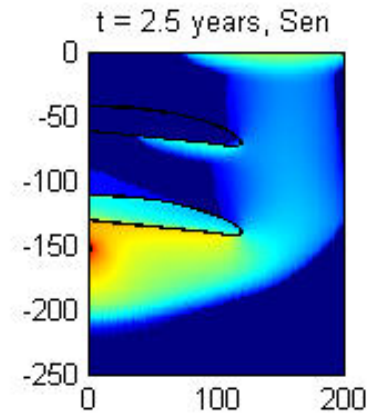
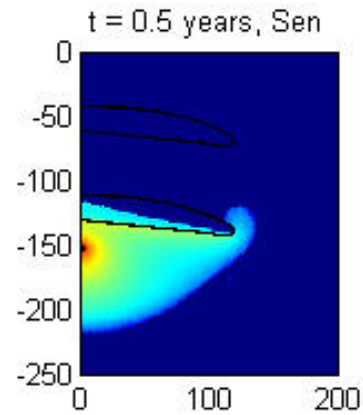
Water Low:
0.05 mPa·s

CO₂ high:
0.5 mPa·s

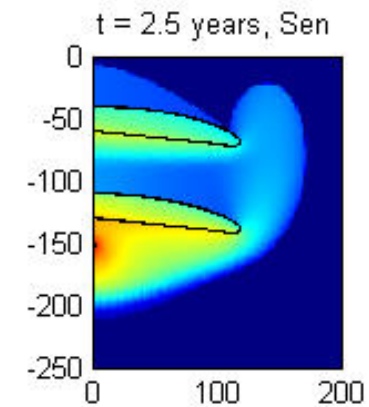
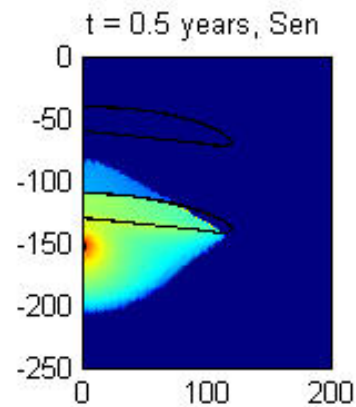


Example 2: Solubility trapping

No-dissolution

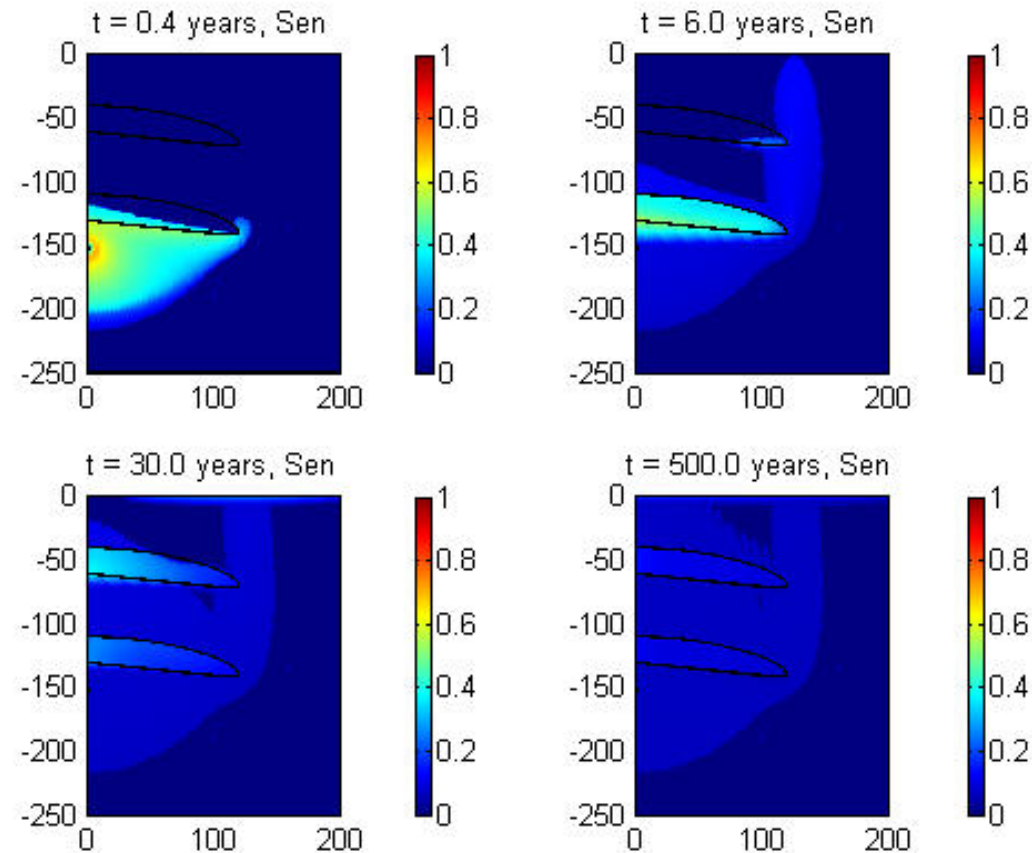


Dissolution

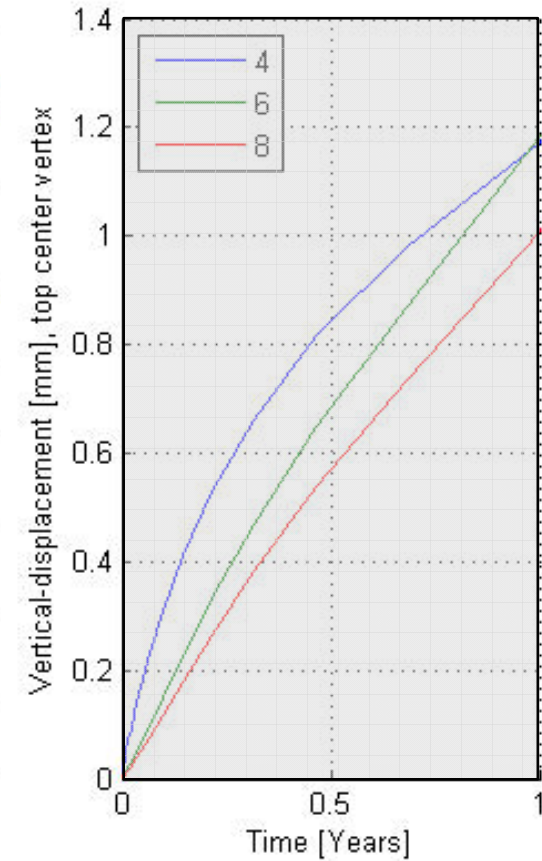
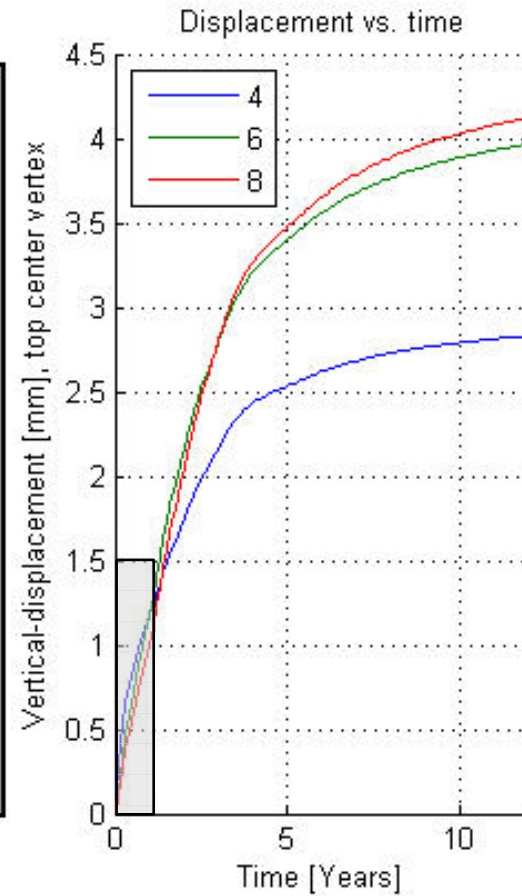
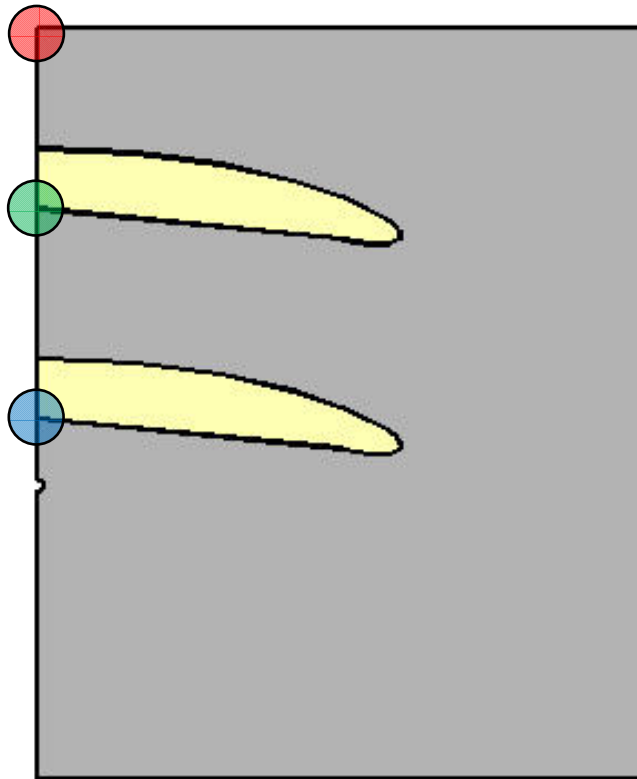


Example 3: Residual trapping

($S_{r,CO_2} = 0.05$)

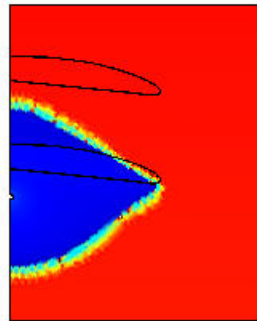


Example 4: Poroelasticity

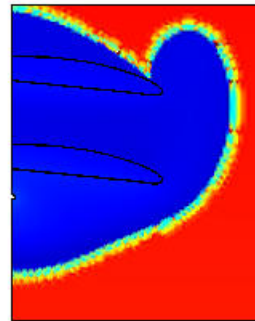


Example 5: Calculating pH

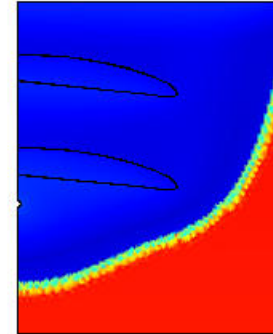
t = 0.5 years, pH
Min: 3.1, max: 5.1



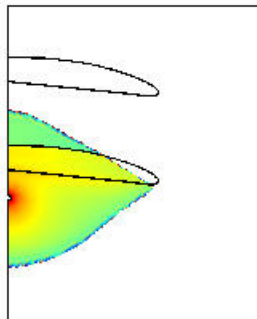
t = 2.5 years, pH
Min: 3.1, max: 5.1



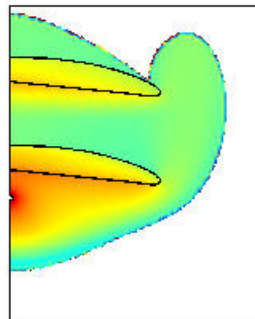
t = 10.0 years, pH
Min: 3.1, max: 5.1



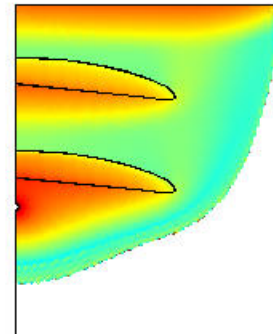
t = 0.5 years, pH
Min: 3.0, max: 3.5



t = 2.5 years, pH
Min: 3.0, max: 3.5



t = 10.0 years, pH
Min: 3.0, max: 3.5



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Conclusion

- A robust model (2D and axial symmetric) that considers many main features related to CO₂ injection
 - More chemical reactions to be added
 - More realistic material models (poroelasticity)
- Most important storage mechanisms:
 - Residual and solubility trapping
- Remaining tasks:
 - Verification (planned lab-experiment summer/fall 2009)
 - Simulation of “real-life” cases
- Thank you for you attention!

CO₂ solubility and pK_w

Function data:

% X-data and Y-data, temperature [degC], pressure [MPa]

0.0 25.0 50.0 75.0 100.0 150.0 200.0 250.0 300.0

0.1 25.0 50.0 75.0 100.0 150.0 200.0 250.0 300.0 350.0 400.0 500.0 600.0 700.0 800.0 900.0 1000.0

% Interpolation data

14.946	13.995	13.264	12.696	12.252	11.641	11.31	11.205	11.339
14.848	13.908	13.181	12.613	12.165	11.543	11.189	11.05	11.125
14.754	13.824	13.102	12.533	12.084	11.45	11.076	10.898	10.893
14.665	13.745	13.026	12.458	12.006	11.364	10.974	10.769	10.715
14.58	13.668	12.953	12.385	11.933	11.283	10.88	10.655	10.568
14.422	13.524	12.815	12.249	11.795	11.135	10.713	10.458	10.327
14.278	13.39	12.687	12.123	11.668	11	10.564	10.289	10.131
14.145	13.265	12.567	12.004	11.549	10.876	10.43	10.14	9.963
14.021	13.148	12.453	11.892	11.437	10.76	10.306	10.005	9.814
13.906	13.037	12.346	11.786	11.331	10.651	10.191	9.881	9.679
13.797	12.932	12.243	11.685	11.23	10.548	10.083	9.766	9.555
13.595	12.736	12.052	11.496	11.042	10.356	9.884	9.557	9.332
13.411	12.556	11.875	11.322	10.868	10.181	9.703	9.369	9.135
13.24	12.389	11.71	11.159	10.705	10.018	9.537	9.197	8.956
13.08	12.233	11.556	11.006	10.553	9.865	9.381	9.037	8.791
12.93	12.085	11.41	10.861	10.41	9.721	9.236	8.888	8.638
12.788	11.946	11.272	10.725	10.273	9.585	9.098	8.748	8.495

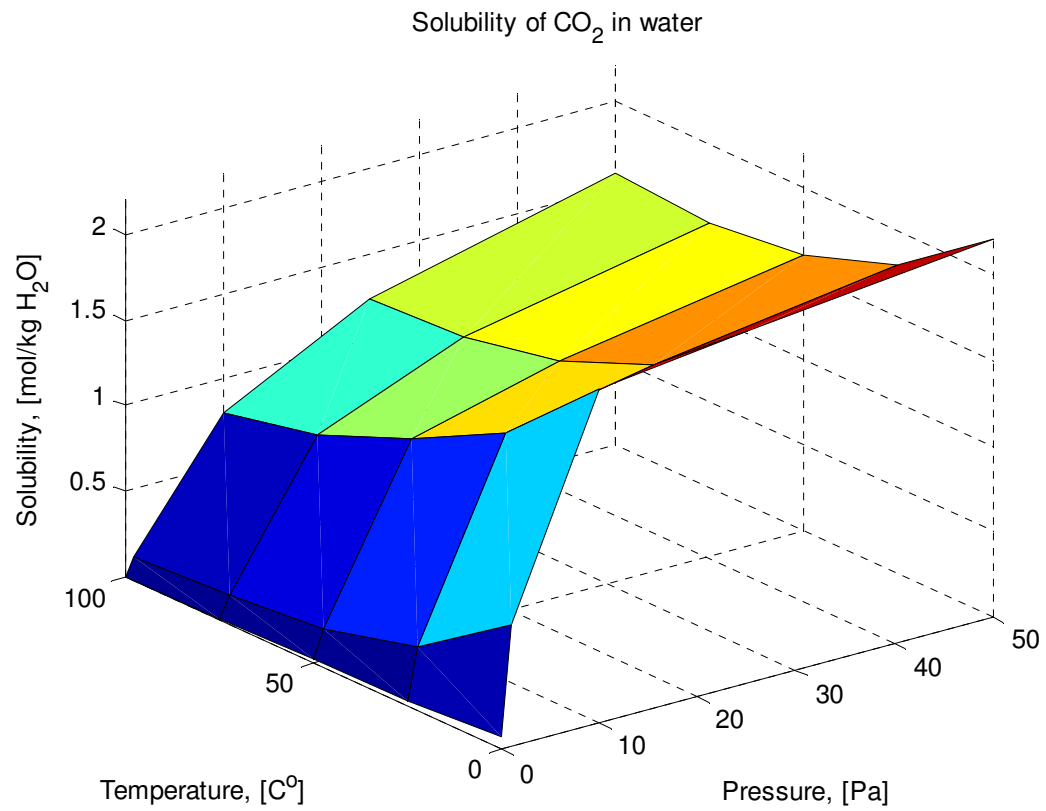
% X-data and Y-data, pressure [Pa], temperature [degC]

0.1 1.0 10.0 25.0 50.0

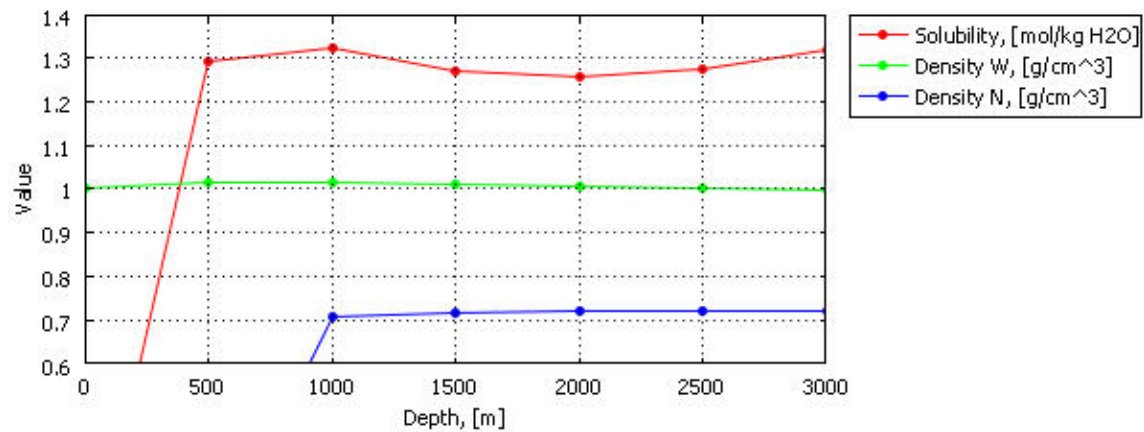
0.0 25.0 50.0 75.0 100.0

% Interpolation data, solubility [mol/kg H2O]

0.08	0.72	1.95	2.06	2.21
0.03	0.33	1.45	1.61	1.81
0.02	0.19	1.16	1.38	1.61
0.01	0.13	0.93	1.27	1.55
0.0010	0.1	0.8	1.24	1.58



Solubility of CO₂ in water as function of temperature (°C) and pressure (MPa)



Plots of solubility of CO₂ in water and density of CO₂ and water plotted as a function of depth (taking pressure and temperature variations into account). Pressure gradient is app. 10000 [Pa/m] and the temperature gradient is 28 [K/km].